Fe-Cu-REE U-Pb

*

Re-Os

1 2	1**	1	1	3	1	1 2	1 2
YE XianTao ^{1 2}	ZHU WeiGuang ¹ **	ZHONG Hong ¹	HE DeFeng ¹	REN Tao ³	BAI ZhongJie ¹	FAN HongPeng ¹	² and HU WenJun ¹ ²
1.				550002			
2.	100049						
3.		650093					
1.						55000	2
2.							

					LA-ICP-I	MS U-Pb	
			Th/U	J > 0. 4		200	
$^{207}\mathrm{Pb}/^{206}\mathrm{Pb}$		1.75 ~ 1.88Ga	1.90 ~ 2.00G	a 2.02 ~ 2.20G	a 2.30 ~ 2.4	40Ga	3. 0Ga
	1750Ma				1. 7Ga		
		Re-Os			6	Re-O	s
1690 ±	99Ma MSWD =	9.0		$1685 \pm 37 Ma$	MSWD = 3.0)	
1. 7Ga							
		REE					
_		Ithe		1 7Ga			_
				1.704	1.70%	Columbia	
		-			1. / Ga	Columbia	
	TT I	D L 1	Pa Oa				
 D5	U-1	11	ne-Os				
P.J	95 F397.5 F0	11					
				2002			
				2002			
1							
1			2	,			
	-		2	-			
1996	IOCG	iron oxide-coppe	er-gold				
Greentree	2007 Zhao 2	2010 Zhao and	Zhou		1		
2011		-		-			
						Greentree and Li 2	2008
-	2004				Zhao	2010	
			2	.009			
2004 2005 Greentre	e and Li 2008	Zhao 201	0 Zhao 1	990 Hu	1991	-	
and Zhou 2011 Zha	o 2012	Chen and Zhou	2012	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	.,,,		
	-	1 7Ca	2012		∐_Ph		
		1.70a		$1687 \pm 8M_{\odot}$	2008	1675 + 8Ma Croontru	
2008	2000 Croontro	and 1; 2008 7	haa and	1007 ± 0141a	2008	1075 ± 6 ma Greenum	ie
Z000 Zhou 2011 Chon and	d Zhou 2012						
Zhou 2011 Chen and	u Zhou 2012						
		-					
1007							
1997	1000	1000	1000				
1984	1990	1993	1993				
1997	1999	200	01				
	-						
	Fe-Cu	-REE					
		LA-ICF	P-MS U-				
Pb							
Re-Os							
-							
		1. 7Ga					

Columbia

1. / G

Rogers and Santosh 2002 Zhao







1990

Fig. 3 Simplified geological map of the Yinachang deposit in Wuding County Yunnan Province after Wu 1990



4

LA-ICP-MS U-Pb DFH1101 N 25°32'53. 1" E 102°13'34. 3" DFH1102 N 25°32'53. 1" E 102°13'34. 3"

CL

U-Pb

4 a -

3

DFH1101 b - DFH1102

Q22c-13 ((63050626j)Tj 003 1dTf 0 Tr 8.830188 0 0 8.830188 0 -7.50566 Tm 40.103464.23.24638 75183001)T554945 0 TD (. tuff- breccia-

Fig. 4 Photographs and photomicrographs of the representative

tuff a c and breccias b d from the Yinachang deposit



a b - c d - e - f - g - h i - . Ccp- Cal- Py- Mgt- Ap- Qtz- WR-

Fig. 5 Photographs and photomicrographs of iron-copper ore from the Yinachang deposit

 $a \ b \ \text{-vein-type ore} \ c \ d \ \text{-bedded ore} \ e \ \text{-disseminated ore} \ f \ \text{-apatite and calcite in the ore} \ g \ \text{-calcite in the magnetite ore} \ h \ \text{-calcite in the magnetite ore} \ h \ \text{-calcite in the magnetite ore} \ h \ \text{-calcite in the wall-rock}$ the copper ore i -calcite in the wall-rock. Ccp-chalcopyrite Cal-calcite Py-pyrite Mgt-magnetite Ap-apatite Qtz-quartz WR-wall-rock



ICP-MS 91500 GJ-1 Plešovice U-Pb NIST SRM 610 Si Pb Zr Liu 2010a Hu 2011 **ICPMSDataCal** Liu 2010a b $40 \sim 60$ 99% 200 Re-Os 2010 ELAN DRC-e ICP-MS Qi $^{185}\,\mathrm{Re}$ 0.1g 190 Os 200℃ 12h Os Os $3 \mathrm{mL}$ 2mol/L HCl

Fig. 6 Representative CL images of the detrital zircon grains for tuff and breccia from the Yinachang deposit

 AG 1-X8
 Re
 Qi
 2007
 2010

 3mL
 ICP-MS
 RSD%
 3%

LA-ICP-MS U-Pb

1 Table 1 LA-ICP-MS zirco

deposit
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analyses
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zircon
A-ICP-MS
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		$\times 10^{-6}$		TL .11									M	E E			
	Pb	Πh	n	Ih/ U	$^{207}{\rm Pb}/^{206}{\rm Pb}$	1σ	$^{207}{\rm Pb}/^{235}{\rm U}$	1σ	$^{206}\mathrm{Pb}/^{238}\mathrm{U}$	1σ	$^{207}{\rm Pb}/^{206}{\rm Pb}$	1σ	$^{207}{ m Pb}/^{235}{ m U}$	1σ	$^{206}{\rm Pb}/^{238}{\rm U}$	1σ	
DFH1101																	
- 01	152.7	274	352	0.78	0.1089	0.0029	5.0129	0.1233	0.3251	0.0064	1781	48	1822	21	1815	31	%66
- 02	123.9	133	276	0.48	0.1356	0.0014	7.0601	0.0762	0.3757	0.0023	2172	18	2119	10	2056	11	96%
- 03	95.4	152	219	0.69	0.1186	0.0012	5.7333	0.0613	0.3492	0.0021	1935	19	1936	6	1931	10	%66
- 04	80.0	128	156	0.82	0.1324	0.0013	7.2370	0.0759	0.3950	0.0026	2131	13	2141	6	2146	12	%66
- 05	91.7	98	176	0.56	0.1431	0.0014	8.4020	0.0842	0.4240	0.0025	2265	18	2275	6	2279	11	%66
- 06	54.7	66.0	111	0.60	0.1325	0.0015	7.4449	0.0840	0.4054	0.0028	2132	14	2166	10	2194	13	98%
- 07	98.9	85.7	166	0.52	0.1521	0.0020	10.0328	0.1323	0.4764	0.0031	2369	23	2438	12	2512	13	<i>%L6</i>
- 08	221.3	119	703	0.17	0.1074	0.0015	4.5076	0.0628	0.3019	0.0022	1755	26	1732	12	1701	11	98%
- 00	137.0	179	307	0.58	0.1244	0.0014	6.4374	0.0710	0.3727	0.0022	2020	- 14	2037	10	2042	10	%66
- 10	67.5	101	172	0.59	0.1096	0.0012	5.1086	0.0595	0.3363	0.0022	1794	21	1838	10	1869	11	98%
- 11	88.0	69.5	172	0.40	0.1416	0.0014	8.7017	0.0874	0.4426	0.0027	2247	17	2307	6	2362	12	<i>%10</i>
- 12	92.6	76	187	0.52	0.1409	0.0013	8.3040	0.0828	0.4251	0.0028	2239	16	2265	6	2284	12	%66
- 13	53.1	98	156	0.63	0.1090	0.0020	4.5260	0.0816	0.2989	0.0026	1783	33	1736	15	1686	13	<i>%10</i>
- 14	151.6	45.3	297	0.15	0.1359	0.0032	8.5099	0.1912	0.4487	0.0041	2176	8	2287	20	2389	18	95%
- 15	48.3	78	118	0.66	0.1074	0.0030	4.8496	0.1339	0.3217	0.0037	1755	52	1794	23	1798	18	%66
- 16	88.3	113	193	0.58	0.1344	0.0012	7.1352	0.0668	0.3823	0.0020	2167	15	2128	×	2087	6	98%
- 17	141.2	121	309	0.39	0.1418	15	2128				8					0	

		$\times 10^{-6}$											M	a			
	Pb	Th	n	Th/U	$^{207}{\rm Pb}/^{206}{\rm Pb}$	1σ	$^{207}{\rm Pb}/^{235}{\rm U}$	1σ	$^{206}\mathrm{Pb}/^{238}\mathrm{U}$	1σ	$^{207}\mathrm{Pb}/^{206}\mathrm{Pb}$	1σ	$^{207}{\rm Pb}/^{235}{\rm U}$	1σ	$^{206}{\rm Pb}/^{238}{\rm U}$	$ \sigma $	
- 36	80.9	209	142	1.47	0.1200	0.0013	6.3927	0.0761	0.3834	0.0029	1967	19	2031	10	2092	14	9/2/6
- 37	87.2	64.5	167	0.39	0.1413	0.0014	8.6286	0.0934	0.4396	0.0030	2243	18	2300	10	2349	13	979%
- 38	266.3	264	713	0.37	0.1105	0.0011	5.0255	0.0526	0.3267	0.0018	1809	19	1824	6	1822	6	%66
- 39	101.1	93.2	236	0.39	0.1188	0.0014	6.0271	0.0729	0.3643	0.0026	1939	21	1980	11	2002	12	98%
- 40	103.0	84.7	196	0.43	0.1444	0.0018	8.8538	0.1100	0.4396	0.0031	2280	21	2323	11	2349	14	98%
- 41	69.0	74.6	135	0.55	0.1341	0.0016	7.6710	0.0938	0.4103	0.0030	2154	20	2193	П	2216	13	98%
- 42	88.9	142	212	0.67	0.1095	0.0012	5.1544	0.0604	0.3375	0.0023	1792	20	1845	10	1875	11	98%
- 43	89.6	89.3	210	0.43	0.1452	0.0015	7.1268	0.0931	0.3524	0.0035	2300	17	2127	12	1946	17	91%
- 44	266.3	264	713	0.37	0.1103	0.0010	4.9246	0.0457	0.3202	0.0017	1806	16	1806	8	1791	8	%66
- 45	161.9	170	312	0.55	0.1391	0.0013	8.2752	0.0886	0.4270	0.0031	2217	16	2262	10	2292	14	98%
- 46	129.0	253	289	0.87	0.1203	0.0012	5.6090	0.0600	0.3350	0.0022	1961	23	1917	6	1863	10	9/2/26
- 47	211.5	374	438	0.85	0.1389	0.0014	7.5703	0.0909	0.3905	0.0031	2213	18	2181	11	2125	14	9/2/26
- 48	109.7	155	230	0.67	0.1260	0.0013	6.6323	0.0745	0.3783	0.0027	2044	18	2064	10	2068	12	%66
- 49	173.7	177	327	0.54	0.1434	0.0013	8.7362	0.0925	0.4378	0.0031	2269	15	2311	10	2341	14	98%
- 50	137.0	125	343	0.36	0.1169	0.0011	5.4973	0.0531	0.3382	0.0019	1910	18	1900	8	1878	6	98%
-51	215.8	177	347	0.51	0.1799	0.0016	12.2556	0.1307	0.4904	0.0041	2654	14	2624	10	2573	18	98%
- 52	98.4	41.0	157	0.26	0.1785	0.0017	12.9855	0.1377	0.5232	0.0036	2639	11	2679	10	2713	15	98%
- 53	48.7	68.7	120	0.57	0.1068	0.0013	4.8869	0.0608	0.3302	0.0027	1746	22	1800	10	1839	13	<i>%16</i>
- 54	106.4	109	195	0.56	0.1406	0.0015	8.4237	0.0995	0.4313	0.0031	2236	19	2278	11	2312	14	%86
- 55	134.8	120	308	0.39	0.1266	0.0013	6.5019	0.0767	0.3693	0.0027	2052	19	2046	10	2026	13	%66
- 56	73.4	196	140	1.40	0.1222	0.0014	5.9134	0.0683	0.3483	0.0022	1989	20	1963	10	1926	10	98%
- 57	62.0	70.0	119	0.59	0.1379	0.0014	7.9104	0.0866	0.4133	0.0028	2211	17	2221	10	2230	13	%66
- 58	36.1	69.7	74.7	0.93	0.1208	0.0016	6.0204	0.0861	0.3598	0.0031	1969	23	1979	12	1981	15	%66
- 59	82.1	263	167	1.58	0.1116	0.0013	5.0164	0.0616	0.3236	0.0023	1828	21	1822	10	1807	11	%66
- 60	187.0	197	354	0.56	0.1432	0.0015	8.3718	0.0911	0.4207	0.0027	2266	18	2272	10	2264	12	%66
-61	49.4	77.2	82.9	0.93	0.1454	0.0019	8.8411	0.1230	0.4378	0.0035	2294	23	2322	13	2341	16	%66
- 62	123.4	92.1	250	0.37	0.1429	0.0015	8.1120	0.0905	0.4081	0.0025	2263	19	2244	10	2206	12	98%
- 63	215.1	194	431	0.45	0.1451	0.0014	8.2793	0.0852	0.4102	0.0023	2289	17	2262	6	2216	10	9/2/56
- 64	133.9	124	299	0.42	0.1377	0.0014	7.0855	0.0792	0.3696	0.0026	2198	18	2122	10	2028	12	95%
- 65	160.0	132	332	0.40	0.1434	0.0014	7.9348	0.0791	0.3978	0.0024	2269	17	2224	6	2159	11	<i>%16</i>
- 66	79.1	70.6	174	0.41	0.1253	0.0014	6.7131	0.0808	0.3852	0.0028	2035	20	2074	11	2101	13	98%
- 67	62.0	61.8	109	0.57	0.1456	0.0017	9.2008	0.1131	0.4555	0.0035	2295	20	2358	11	2420	16	9/2/56
- 68	63.2	77.5	159	0.49	0.1106	0.0014	5.2508	0.0704	0.3418	0.0027	1810	23	1861	11	1895	13	98%
- 69	123.9	94.3	238	0.40	0.1459	0.0017	8.7938	0.1075	0.4335	0.0030	2298	19	2317	11	2321	13	%66
- 70	151.1	340	302	1.13	0.1213	0.0013	6.1160	0.0688	0.3626	0.0024	1976	14	1993	10	1994	11	%66
- 71	63.0	75.0	117	0.64	0.1443	0.0016	8.6918	0.0966	0.4329	0.0027	2279	19	2306	10	2319	12	%66

		× 10	9	111, 711									N	la			
	Pb	Th	n	Ih/U	$^{207}{\rm Pb}/^{206}{\rm Pb}$	1σ	$^{207}{\rm Pb}/^{235}{\rm U}$	1σ	$^{206}\mathrm{Pb}/^{238}\mathrm{U}$	1σ	$^{207}{\rm Pb}/^{206}{\rm Pb}$	1σ	$^{207}{\rm Pb}/^{235}{\rm U}$	1σ	$^{206}\mathrm{Pb}/^{238}\mathrm{U}$	1σ	
- 72	136.9	136	207	0.66	0.1845	0.0018	13.0323	0.1292	0.5076	0.0030	2694	16	2682	6	2646	13	98%
- 73	122.1	150	231	0.65	0.1418	0.0014	8.3021	0.0890	0.4200	0.0027	2250	50	2265	10	2260	12	%66
- 74	144.7	227	264	0.86	0.1328	0.0013	7.7595	0.0846	0.4192	0.0030	2135	18	2204	10	2257	13	<i>%16</i>
- 75	156.1	143	353	0.41	0.1297	0.0013	6.7816	0.0713	0.3749	0.0023	2094	23	2083	6	2052	11	98%
- 76	118.4	169	291	0.58	0.1080	0.0013	5.0668	0.0618	0.3367	0.0025	1766	21	1831	10	1871	12	9/2/26
- 77	88.2	103	166	0.62	0.1408	0.0015	8.5921	0.1031	0.4386	0.0035	2237	19	2296	11	2344	16	9796
- 78	123.2	151	277	0.55	0.1193	0.0012	6.1333	0.0680	0.3691	0.0027	1946	18	1995	10	2025	13	98%
- 79	64.8	96.5	133	0.72	0.1243	0.0013	6.7847	0.0806	0.3925	0.0030	2020	- 14	2084	11	2134	14	9796
- 80	63.0	109	151	0.73	0.1084	0.0012	5.1333	0.0626	0.3408	0.0026	1773	20	1842	10	1890	12	9/2/26
- 81	143.8	111	303	0.37	0.1296	0.0012	7.3295	0.0815	0.4065	0.0031	2094	17	2152	10	2199	14	9/2/26
- 82	64.1	65.3	119	0.55	0.1442	0.0016	8.8574	0.1082	0.4419	0.0035	2280	20	2323	11	2359	16	98%
- 83	133.1	168	286	0.59	0.1379	0.0014	7.1239	0.0875	0.3709	0.0030	2211	17	2127	11	2034	14	95%
- 84	79.6	109	182	0.60	0.1162	0.0014	5.7745	0.0709	0.3580	0.0025	1898	22	1943	11	1973	12	98%
FH1102																	
- 01	87.6	164	200	0.82	0.1092	0.0012	4.9917	0.0618	0.3287	0.0025	1787	22	1818	10	1832	12	%66
- 02	24.28	34.6	56.9	0.61	0.1103	0.0016	5.2812	0.0836	0.3466	0.0035	1806	21	1866	14	1918	17	977%
- 03	36.8	62	91	0.68	0.1074	0.0016	4.8210	0.0728	0.3235	0.0029	1767	27	1789	13	1807	14	98%
- 04	213.4	230	468	0.49	0.1435	0.0012	7.1364	0.0634	0.3575	0.0017	2270	15	2129	8	1971	8	92%
- 05	113.9	114	219	0.52	0.1338	0.0012	7.5570	0.0714	0.4069	0.0024	2148	17	2180	8	2201	11	%66
- 06	62.8	91.4	112	0.82	0.1548	0.0016	8.9171	0.1226	0.4145	0.0041	2399	18	2330	13	2235	19	95%
- 07	53.3	122	120	1.01	0.1100	0.0013	4.8264	0.0546	0.3159	0.0018	1811	16	1790	10	1770	6	98%
- 08	74.5	104	153	0.68	0.1303	0.0015	6.7038	0.0784	0.3709	0.0025	2102	20	2073	10	2034	12	98%
- 00	123.5	154	249	0.62	0.1334	0.0014	6.9575	0.0832	0.3754	0.0031	2143	19	2106	11	2055	14	977%
- 10	252.0	284	451	0.63	0.1475	0.0018	8.1843	0.0999	0.3968	0.0026	2317	21	2252	11	2154	12	95%
- 11	95.2	86.7	135	0.64	0.1817	0.0017	13.2204	0.1292	0.5231	0.0032	2668	15	2696	6	2712	14	%66
- 12	200.3	67.7	466	0.15	0.1197	0.0012	6.0441	0.0620	0.3623	0.0020	1954	13	1982	6	1993	6	%66
- 13	114.0	107	211	0.51	0.1406	0.0013	8.3927	0.0873	0.4291	0.0030	2235	16	2274	6	2302	13	98%
- 14	85.6	91.3	184	0.50	0.1193	0.0021	6.0186	0.0983	0.3624	0.0029	1946	38	1979	14	1994	14	%66
- 15	49.0	76.3	120	0.64	0.1101	0.0014	5.0646	0.0700	0.3313	0.0029	1811	18	1830	12	1845	14	%66
- 16	75.7	131	156	0.84	0.1193	0.0014	5.9654	0.0721	0.3601	0.0025	1946	21	1971	11	1983	12	%66
- 17	33.53	22.3	49.6	0.45	0.1794	0.0022	13.4050	0.1688	0.5381	0.0045	2647	53	2709	12	2775	19	%L6
- 18	49.4	68.7	121	0.57	0.1094	0.0012	4.9766	0.0554	0.3283	0.0023	1791	20	1815	6	1830	11	%66
- 19	61.6	61.1	122	0.50	0.1368	0.0013	7.6532	0.0773	0.4029	0.0026	2187	17	2191	6	2182	12	%66
- 20	79.6	92.6	181	0.51	0.1188	0.0012	5.8956	0.0590	0.3577	0.0022	1939	23	1961	6	1971	10	%66
-21	49.6	82.1	99.9	0.82	0.1275	0.0013	6.7275	0.0734	0.3794	0.0026	2065	13	2076	10	2073	12	%66
- 22	63.0	62.8	119	0.53	0.1442	0.0015	8.5432	0.0972	0.4267	0.0029	2280	19	2291	10	192.5	13	⁹ /200

Fe-Cu-REE

U-Pb

Re-Os

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		× 10 ⁻⁽	5	111, 111									N	Ia			
	Pb	ЧГ	n	1h/ U	$^{207}{\rm Pb}/^{206}{\rm Pb}$	1σ	$^{207}{\rm Pb}/^{235}{\rm U}$	1σ	$^{206}\mathrm{Pb}/^{238}\mathrm{U}$	1σ	$^{207}\mathrm{Pb}/^{206}\mathrm{Pb}$	1σ	$^{207}{\rm Pb}/^{235}{\rm U}$	1σ	$^{206}\mathrm{Pb}/^{238}\mathrm{U}$	1σ	
- 23	35.9	58.6	90.3	0.65	0.1089	0.0014	4.8011	0.0596	0.3184	0.0022	1781	23	1785	10	1782	11	%66
- 24	124.4	140	328	0.42	0.1102	0.0011	4.8986	0.0548	0.3199	0.0021	1803	19	1802	6	1789	10	%66
- 25	47.3	63.4	83.8	0.76	0.1447	0.0016	8.8049	0.1078	0.4384	0.0033	2284	19	2318	11	2343	15	98%
- 26	251	503	461	1.09	0.1285	0.0011	7.0057	0.0682	0.3922	0.0024	2080	16	2112	6	2133	11	%66
- 27	264.8	149	630	0.24	0.1221	0.0010	6.3192	0.0613	0.3724	0.0023	1987	15	2021	6	2041	11	%66
- 28	115.3	209	253	0.83	0.1194	0.0011	5.8358	0.0601	0.3521	0.0022	1947	17	1952	6	1945	11	%66
- 29	55.2	102	120	0.85	0.1178	0.0013	5.7559	0.0622	0.3521	0.0020	1924	19	1940	6	1945	10	%66
- 30	136.7	271	317	0.85	0.1146	0.0012	5.2842	0.0547	0.3325	0.0020	1873	18	1866	6	1850	10	%66
- 31	30.9	60.8	69.6	0.87	0.1146	0.0016	5.2778	0.0815	0.3321	0.0029	1876	26	1865	13	1849	14	%66
- 32	23.08	50.6	50.6	1.00	0.1181	0.0018	5.4172	0.0837	0.3324	0.0028	1928	27	1888	13	1850	14	9/2/26
- 33	90.2	114	187	0.61	0.1295	0.0013	7.0000	0.0758	0.3890	0.0027	2092	18	2111	10	2118	13	%66
- 34	42.1	58.7	71.3	0.82	0.1465	0.0016	9.0346	0.1112	0.4441	0.0031	2305	19	2342	11	2369	14	98%
- 35	71.6	158	140	1.14	0.1207	0.0013	6.1774	0.0706	0.3686	0.0027	1969	20	2001	10	2023	13	98%
- 36	22.71	23.3	45.7	0.51	0.1330	0.0018	7.4644	0.0996	0.4056	0.0033	2139	23	2169	12	2195	15	98%
- 37	104.1	91.0	198	0.46	0.1424	0.0015	8.4429	0.0923	0.4268	0.0026	2257	19	2280	10	2291	12	%66
- 38	82.6	72.3	159	0.45	0.1431	0.0017	8.4088	0.0993	0.4223	0.0028	2265	21	2276	11	2271	12	%66
- 39	24.67	22.2	50.1	0.44	0.1391	0.0019	7.8226	0.1091	0.4057	0.0034	2216	24	2211	13	2195	16	%66
- 40	70.6	86.8	143	0.61	0.1308	0.0014	7.1540	0.0789	0.3937	0.0026	2109	14	2131	10	2140	12	%66
-41	106.1	115	227	0.51	0.1283	0.0013	6.9709	0.0784	0.3906	0.0028	2076	18	2108	10	2126	13	%66
- 42	63.38	14.7	165	0.09	0.1173	0.0012	5.7424	0.0639	0.3532	0.0024	1917	23	1938	10	1950	11	%66
- 43	61.7	62.6	112	0.56	0.1443	0.0016	8.9434	0.1008	0.4460	0.0029	2279	19	2332	10	2378	13	98%
- 44	70.20	15.1	179	0.08	0.1200	0.0013	6.0008	0.0692	0.3605	0.0026	1967	19	1976	10	1984	12	%66
- 45	33.0	74.6	74.4	1.00	0.1134	0.0015	5.2027	0.0722	0.3307	0.0026	1855	24	1853	12	1842	12	%66
- 46	142.31	13.1	354	0.04	0.1222	0.0013	6.3090	0.0731	0.3724	0.0026	1991	19	2020	10	2041	12	98%
- 47	139.7	181	338	0.54	0.1115	0.0012	5.2756	0.0639	0.3409	0.0026	1825	25	1865	10	1891	12	98%
- 48	83.7	82.5	179	0.46	0.1291	0.0014	6.9444	0.0832	0.3890	0.0028	2087	14	2104	11	2118	13	%66
- 49	37.6	80.0	83.1	0.96	0.1142	0.0015	5.3632	0.0736	0.3401	0.0028	1933	24	1879	12	1887	13	%66
- 50	79.5	72.0	143	0.50	0.1502	0.0014	9.3526	0.0946	0.4493	0.0029	2350	16	2373	6	2392	13	%66
-51	90.4	65.8	137	0.48	0.1860	0.0018	13.3917	0.1384	0.5196	0.0033	2706	17	2708	10	2697	14	%66
- 52	76.6	135	197	0.68	0.1110	0.0012	4.7530	0.0564	0.3088	0.0019	1817	20	1777	10	1735	10	9/2/6
- 53	69.2	47.5	130	0.	64												

Pb Th U 10^{10} $2^{10}P_{1}/^{206}P_{1}$ 1σ $2^{10}P_{1}/^{206}P_{1}$ 1σ $2^{10}P_{1}/^{206}P_{1}$ 1σ $2^{10}P_{1}/^{206}P_{1}$ 1σ $2^{10}P_{1}/^{20}P_{1}$ 1σ $2^{10}P_{1}/^{20}P_{1}$ 1σ $2^{10}P_{1}/^{20}P_{1}/^{20}P_{1}$ 1σ 2^{11} $2^{11}P_{1}/^{20$			$\times 10^{-6}$											M	a			
-59 31.92 19.8 40.0 0.57 0.197 0.0026 18. -60 55.9 47.1 82.0 0.57 0.1800 0.0016 5. -61 26.04 43.5 61.0 0.71 0.1101 0.0016 5. -63 47.2 55.3 85.2 0.65 0.1457 0.0019 8. -66 29.14 52.5 65.9 0.80 0.1116 0.0014 5. -66 29.14 52.5 65.7 128 130 0.99 0.0114 5. -66 29.14 52.5 65.7 126 0.22 0.0114 5. -70 46.0 42.0 65.7 126 0.22 0.0114 5. -71 59.9 85.4 105 0.72 0.1130 0.0014 5. -77 59.9 81.3 0.72 0.1130 0.0013 5. -77 59.9 81.3 0.7		Pb	Th	n	∩∕ų.I.	$207 \mathrm{Pb}/^{206} \mathrm{Pb}$	1σ	$^{207}{\rm Pb}/^{235}{\rm U}$	1σ	$^{206}\mathrm{Pb}/^{238}\mathrm{U}$	$\frac{1\sigma}{1}$	$207 {\rm Pb}/{\rm 206 Pb}$	1σ	$^{207}\mathrm{Pb}/^{235}\mathrm{U}$	1σ	$^{206}{\rm Pb}/^{238}{\rm U}$	1σ	
-60 55.9 47.1 82.0 0.57 0.1800 0.0020 $13.$ -61 26.04 43.5 61.0 0.711 0.1101 0.0016 5. -63 47.2 55.3 85.2 0.65 0.1457 0.0019 8. -66 29.14 52.5 85.2 0.65 0.1179 0.0012 5. -67 63.2 119 185 0.64 0.1100 0.0012 5. -67 63.2 128 130 0.99 0.1179 0.0014 5. -70 46.0 42.0 66.2 0.64 0.1100 0.0012 5. -71 59.9 85.4 105 0.72 0.1129 0.0014 5. -77 54.9 92.6 0.72 0.1131 0.0012 5. -77 54.9 0.53 0.64 0.1113 0.0014 5. -77 54.9 92	- 59	31.92	19.8	40.0	0.50	0.2197	0.0026	18.8909	0.2486	0.6217	0.0055	2989	19	3036	13	3117	22	9/2/26
-61 26.04 43.5 61.0 0.71 0.1101 0.0016 5. -63 47.2 55.3 85.2 0.65 0.1457 0.0019 81 -64 76.7 119 185 0.64 0.1100 0.0012 5. -65 44.3 70.9 106 0.67 0.1129 0.0014 5. -66 29.14 52.5 65.9 0.80 0.1116 0.0014 5. -67 63.2 128 130 0.99 0.1116 0.0014 5. -70 46.0 42.0 66.2 0.64 0.1110 0.0014 5. -71 59.9 85.4 105 0.22 0.1119 0.0014 5. -77 45.0 66.2 0.64 0.1110 0.0014 5. -77 135.6 53.1 105 0.72 0.1131 0.0014 5. -77 135.6 54.1 156 0	- 60	55.9	47.1	82.0	0.57	0.1800	0.0020	13.4778	0.1675	0.5401	0.0042	2653	18	2714	12	2784	17	9/2/26
-62 112.5 59.0 266 0.22 0.1217 0.0014 65.7 -63 -47.2 55.3 85.2 0.66 0.1457 0.0012 $55.$ -66 -44.3 70.9 106 0.67 0.1129 0.0014 $55.$ -67 63.2 119 185 0.64 0.1116 0.0014 55.7 -67 63.2 1128 130 0.99 0.1116 0.0014 55.7 -70 46.0 42.0 66.2 0.64 0.1129 0.0014 55.7 -77 59.9 85.4 105 0.811 2128 0.722 0.1129 0.0014 55.7 -77 19.44 20.6 95.7 0.722 0.1129 0.0014 57.7 -77 135.6 54.4 105.8 0.720 0.0014 57.7 -77 135.6 54.4	- 61	26.04	43.5	61.0	0.71	0.1101	0.0016	5.1550	0.0768	0.3391	0.0027	1802	26	1845	13	1882	13	98%
-63 47.2 55.3 85.2 0.65 0.1457 0.0019 81 -66 24.3 70.9 106 0.67 0.1129 0.0014 55 -66 29.14 52.5 65.9 0.80 0.1116 0.0014 55 -67 63.2 128 130 0.99 0.1179 0.0014 55 -68 51.6 65.7 126 0.52 0.1110 0.0014 55 -70 46.0 42.0 65.7 126 0.72 0.1100 0.0014 55 -77 59.9 85.4 105 0.72 0.1100 0.0014 57 -77 135.6 54.7 25.8 0.644 0.11129 0.0014 57 -77 135.6 54.7 25.8 0.644 0.1129 0.0014 57 -77 135.6 54.7 255.8 0.644	- 62	112.5	59.0	266	0.22	0.1217	0.0014	6.3109	0.0740	0.3741	0.0024	1981	53	2020	10	2048	11	98%
-64 76.7 119 185 0.64 0.1100 0.0012 5 -66 29.14 52.5 65.9 0.80 0.1116 0.0014 5 -67 63.2 128 130 0.99 0.1179 0.0014 5 -68 51.6 65.7 128 130 0.99 0.1179 0.0014 5 -70 46.0 42.0 65.7 126 0.52 0.1120 0.0014 5 -71 59.9 85.4 105 0.72 0.2020 0.0013 5 -73 19.44 20.6 95.6 0.70 0.1110 0.0013 5 -73 19.44 20.6 95.6 0.70 0.1313 0.0014 5 -73 19.44 20.6 95.6 0.72 0.1129 0.0013 5 -74 43.9 62.1 95.6 0.72 0.1351 0.0013 5 -77 135.6	- 63	47.2	55.3	85.2	0.65	0.1457	0.0019	8.8067	0.1194	0.4369	0.0033	2295	22	2318	12	2337	15	%66
-65 44.3 70.9 106 0.67 0.1129 0.0014 5.5 -67 63.2 128 130 0.99 0.1116 0.0014 5.5 -68 51.6 65.7 126 0.52 0.1116 0.0014 5.5 -70 86.1 82.9 115 0.72 0.2020 0.0014 5.5 -71 59.9 85.4 105 0.81 0.1408 0.0014 5.5 -73 19.44 20.6 92.8 130 0.72 0.1110 0.0013 5.5 -73 19.44 20.6 92.8 130 0.72 0.1110 0.0013 5.5 -75 51.9 81.3 128 0.64 0.1123 0.0013 5.5 -77 135.6 54.7 276 0.20 0.1133 0.0014 5.7 -77 135.6 0.70 0.1129 0.0013 5.7 -78 51.9	- 64	76.7	119	185	0.64	0.1100	0.0012	5.1465	0.0640	0.3371	0.0025	1799	16	1844	Ξ	1873	12	98%
-66 $29, 14$ 52.5 65.9 0.80 0.1116 0.0016 5.5 -67 63.2 128 130 0.99 0.1179 0.0014 5.5 -68 51.6 65.7 126 0.52 0.1179 0.0014 5.5 -70 46.0 42.0 66.2 0.64 0.1836 0.0024 13.5 -71 59.9 85.4 105 0.81 0.1408 0.0014 5.7 -72 54.9 92.8 1005 0.81 0.1408 0.0024 13.5 -77 59.9 85.4 105 0.81 0.1408 0.0014 5.7 -77 135.6 54.7 276 0.254 0.11129 0.0014 5.7 -77 135.6 54.7 276 0.254 0.11346 0.0013 7.7 -78 1173.4 174 0.557 0.11346 <t< td=""><td>- 65</td><td>44.3</td><td>70.9</td><td>106</td><td>0.67</td><td>0.1129</td><td>0.0014</td><td>5.2148</td><td>0.0658</td><td>0.3337</td><td>0.0023</td><td>1847</td><td>23</td><td>1855</td><td>Ξ</td><td>1856</td><td>Π</td><td>%66</td></t<>	- 65	44.3	70.9	106	0.67	0.1129	0.0014	5.2148	0.0658	0.3337	0.0023	1847	23	1855	Ξ	1856	Π	%66
-67 63.2 128 130 0.99 0.1179 0.0014 5.1 -68 51.6 65.7 126 0.52 0.1120 0.0014 5.5 -70 46.0 42.0 66.2 0.64 0.1836 0.0024 15. -71 59.9 85.4 105 0.81 0.1408 0.0014 5. -72 54.9 92.8 100 66.2 0.64 0.1836 0.0023 13. -73 19.44 20.6 92.6 0.70 0.1110 0.0014 5. -75 52.0 69.6 99.6 0.70 0.11129 0.0014 5. -77 135.6 54.7 276 0.23 0.1420 0.0014 5. -77 135.6 54.7 276 0.24 0.1139 0.0013 7. -78 113.5 0.54 0.64 0.1346 0.0014 5. -78 132.0 69.6	- 66	29.14	52.5	65.9	0.80	0.1116	0.0016	5.2541	0.0746	0.3412	0.0024	1825	26	1861	12	1892	12	98%
-68 51.6 65.7 126 0.52 0.1120 0.0014 5.3 -70 46.0 42.0 66.2 0.64 0.1836 0.0022 13. -71 39.9 85.4 105 0.81 0.1408 0.0013 5. -72 54.9 92.8 130 0.72 0.1450 0.0013 5. -73 19.44 20.6 35.7 0.58 0.1450 0.0014 5. -75 51.9 81.3 128 0.64 0.1119 0.0014 5. -75 52.0 69.6 99.6 0.70 0.1313 0.0015 7. -77 135.6 54.7 276 0.20 0.1420 0.0016 8. -77 135.6 54.7 276 0.1115 0.0014 5. -78 48.6 53.1 99.1 0.54 0.1116 0.0013 7. -81 173.4 174 227 <td< td=""><td>- 67</td><td>63.2</td><td>128</td><td>130</td><td>0.99</td><td>0.1179</td><td>0.0014</td><td>5.8883</td><td>0.0706</td><td>0.3604</td><td>0.0025</td><td>1925</td><td>20</td><td>1960</td><td>10</td><td>1984</td><td>12</td><td>98%</td></td<>	- 67	63.2	128	130	0.99	0.1179	0.0014	5.8883	0.0706	0.3604	0.0025	1925	20	1960	10	1984	12	98%
-69 86.1 82.9 115 0.72 0.2020 0.0024 15. -71 59.9 85.4 105 0.81 0.1408 0.0016 8.3 -71 59.9 85.4 105 0.81 0.1408 0.0013 5.3 -73 19.44 20.6 35.7 0.58 0.1450 0.0013 5.3 -75 51.9 81.3 128 0.64 0.1119 0.0014 5.6 -75 53.1 99.6 0.70 0.1313 0.0014 5.7 -77 135.6 54.7 276 0.20 0.0014 5.7 -77 135.6 54.7 276 0.20 0.0014 5.7 -78 48.6 53.1 99.1 0.54 0.1129 0.0014 5.7 -79 79.1 93.5 154 0.64 0.1131 0.0014 5.7 -79 79.1<	- 68	51.6	65.7	126	0.52	0.1120	0.0014	5.2242	0.0701	0.3365	0.0025	1832	23	1857	Ξ	1870	12	%66
-70 46.0 42.0 66.2 0.64 0.1836 0.0022 $13.$ -71 59.9 85.4 105 0.81 0.1408 0.0015 $5.5.7$ -72 54.9 92.8 130 0.72 0.1110 0.0015 $5.5.7$ -73 19.44 20.6 35.77 0.58 0.1450 0.0014 $5.5.7$ -75 52.0 69.6 99.6 0.70 0.1129 0.0014 $5.7.7$ -77 135.6 54.7 276 0.20 0.1420 0.0014 $5.7.7$ -77 135.6 54.7 276 0.20 0.1129 0.0014 $5.7.7$ -77 135.6 54.7 276 0.20 0.11324 0.0014 $5.7.7$ -79 79.1 92.7 0.79 0.1324 0.0014 $5.7.7$ -80 105.7 2131 227 0.84	- 69	86.1	82.9	115	0.72	0.2020	0.0024	15.5602	0.1927	0.5550	0.0039	2842	14	2850	12	2846	16	%66
-71 59.9 85.4 105 0.81 0.1408 0.0016 8. -72 54.9 92.8 130 0.72 0.1110 0.0013 5. -73 19.44 20.6 35.7 0.58 0.1450 0.0013 5. -74 43.9 62.1 96.8 0.64 0.1129 0.0014 5. -77 51.9 81.3 128 0.64 0.1115 0.0014 5. -77 135.6 54.7 276 0.20 0.1420 0.0015 7. -77 135.6 54.7 276 0.20 0.1420 0.0014 5. -77 135.6 54.7 276 0.20 0.1324 0.0015 7. -79 79.1 93.5 154 0.61 0.1324 0.0015 7. -79 131 236 0.56 0.1476 0.0013 7. -81173.4 1055.7 227	- 70	46.0	42.0	66.2	0.64	0.1836	0.0022	13.5549	0.1696	0.5334	0.0044	2687	20	2719	12	2756	19	98%
-72 54.9 92.8 130 0.72 0.1110 0.0013 $5.$ -73 19.44 20.6 35.7 0.58 0.1450 0.0013 $5.$ -74 43.9 62.1 96.8 0.64 0.1119 0.0014 5.6 -75 51.0 69.16 99.6 0.70 0.1313 0.0014 5.7 -76 51.9 81.3 128 0.64 0.1115 0.0014 5.7 -77 135.6 54.7 276 0.20 0.1420 0.0014 5.7 -79 79.1 93.5 154 0.61 0.1324 0.0018 7.6 -80 105.5 131 236 0.56 0.1191 0.0012 5.7 -80 105.5 131 236 0.56 0.1191 0.0012 5.7 -80 157.4 0.64 0.1324 0.0013 <td>- 71</td> <td>59.9</td> <td>85.4</td> <td>105</td> <td>0.81</td> <td>0.1408</td> <td>0.0016</td> <td>8.4530</td> <td>0.1001</td> <td>0.4327</td> <td>0.0031</td> <td>2237</td> <td>20</td> <td>2281</td> <td>11</td> <td>2318</td> <td>14</td> <td>98%</td>	- 71	59.9	85.4	105	0.81	0.1408	0.0016	8.4530	0.1001	0.4327	0.0031	2237	20	2281	11	2318	14	98%
-73 $19, 44$ $20, 6$ $35, 7$ 0.58 0.1450 0.0014 5.6 -74 43.9 62.1 96.8 0.64 0.1129 0.0014 5.6 -76 51.9 81.3 128 0.64 0.1115 0.0014 5.6 -76 51.9 81.3 128 0.64 0.1115 0.0014 5.7 -76 51.9 81.3 128 0.64 0.1115 0.0018 7.6 -79 79.1 93.5 154 0.61 0.1321 0.0018 7.6 -80 105.5 131 236 0.56 0.1191 0.0012 5.7 -81 173.4 174 320 0.54 0.1191 0.0012 5.7 -81 173.4 174 320 0.56 0.1191 0.0012 5.7 -82 150.7 227 284.7 0.62	- 72	54.9	92.8	130	0.72	0.1110	0.0013	5.1143	0.0623	0.3320	0.0023	1817	21	1838	10	1848	11	%66
-74 43.9 62.1 96.8 0.64 0.1129 0.0014 5.1 -75 52.0 69.6 99.6 0.70 0.1115 0.0014 5.1 -77 51.9 81.3 128 0.64 0.1115 0.0014 5.1 -77 135.6 54.7 276 0.20 0.1420 0.0018 7.5 -79 79.1 93.5 154 0.61 0.1324 0.0018 7.7 -80 105.5 131 236 0.56 0.1191 0.0012 7.7 -81 173.4 174 320 0.54 0.1191 0.0012 5.7 -81 173.4 174 320 0.56 0.1113 0.0012 5.1 -83 160.0 213 247 0.62 0.1113 0.0012 5.1 -83 160.0 213 0.59 0.1136	- 73	19.44	20.6	35.7	0.58	0.1450	0.0021	8.8198	0.1403	0.4382	0.0042	2289	24	2320	15	2343	19	%66
-75 52.0 69.6 97.6 0.115 0.0015 7.7 -77 135.6 54.7 276 0.20 0.1420 0.0014 5.6 -77 135.6 54.7 276 0.20 0.1420 0.0016 8.3 -79 48.6 53.1 99.1 0.54 0.11324 0.0015 7.6 -80 105.5 131 236 0.56 0.1191 0.0012 5.7 -81 173.4 174 320 0.54 0.1191 0.0013 7.7 -82 150.7 227 284 0.80 0.1136 0.0013 7.7 -83 160.0 213 347 0.62 0.1113 0.0013 7.7 -83 160.0 213 0.79 0.0014 5.0 -83 160.0 213 0.64 0.1113 0.0013 5.6	- 74	43.9	62.1	96.8	0.64	0.1129	0.0014	5.6604	0.0775	0.3616	0.0032	1847	18	1925	12	1990	15	96%
-76 51.9 81.3 128 0.64 0.1115 0.0014 51.6 -77 135.6 54.7 276 0.20 0.1420 0.0018 71.6 -79 48.6 53.1 99.1 0.54 0.1351 0.0018 71.6 -79 79.1 93.5 154 0.61 0.1324 0.0015 71.6 -80 105.5 131 236 0.54 0.1191 0.0013 71.6 -81 173.4 174 320 0.54 0.1476 0.0014 51.7 -82 150.7 227 284 0.80 0.11346 0.0013 71.6 -83 160.0 213 347 0.62 0.1270 0.0014 55.7 -84 54.6 132 0.64 0.1113 0.0014 55.7 -88 44.9 35.57 0.20 0.200 0.0014 55.7 -88 44.90 36.5 0.27	- 75	52.0	69.6	9.66	0.70	0.1313	0.0015	7.4376	0.0966	0.4073	0.0032	2117	21	2166	12	2202	15	98%
-77 135.6 54.7 276 0.20 0.1420 0.0016 8.5 -78 48.6 53.1 99.1 0.54 0.1351 0.0018 7.5 -79 79.1 93.5 154 0.61 0.1324 0.0015 7.5 -80 105.5 131 236 0.56 0.1191 0.0012 5.5 -81 173.4 174 320 0.54 0.1476 0.0013 7.6 -82 150.7 227 284 0.80 0.1346 0.0013 7.6 -83 160.0 213 347 0.62 0.1203 0.0014 5.6 -83 160.0 213 347 0.62 0.1203 0.0014 5.6 -86 111.2 68.5 70.9 0.80 0.1136 0.0014 5.6 -87 30.4 56.5 70.9 0.80 0.1136 0.0014 5.6 -88 44.9 9.5 <	- 76	51.9	81.3	128	0.64	0.1115	0.0014	5.0472	0.0683	0.3250	0.0023	1833	18	1827	11	1814	11	%66
-78 48.6 53.1 99.1 0.54 0.1351 0.0018 7.5 -79 79.1 93.5 154 0.61 0.1324 0.0015 7.5 -80 105.5 131 236 0.56 0.1191 0.0015 7.5 -81 173.4 174 320 0.54 0.1476 0.0013 7.5 -82 150.7 227 284 0.80 0.1346 0.0013 7.5 -83 160.0 213 347 0.62 0.1476 0.0014 5.6 -84 54.5 70.9 0.80 0.1136 0.0014 5.6 -88 44.9 36.5 70.9 0.80 0.1136 0.0014 5.7 -88 44.90 36.6 9.74 0.38 0.1276 0.0014 5.7 -90 143 0.59 0.1270 0.0014 5.7	- <i>TT</i>	135.6	54.7	276	0.20	0.1420	0.0016	8.3715	0.0974	0.4228	0.0028	2254	20	2272	Ξ	2273	13	%66
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	- 78	48.6	53.1	99.1	0.54	0.1351	0.0018	7.4327	0.1073	0.3946	0.0031	2165	23	2165	13	2144	14	%66
-80 105.5 131 236 0.56 0.1191 0.0012 5.9 -81 173.4 174 320 0.54 0.1476 0.0014 9.0 -82 150.7 227 284 0.80 0.1346 0.0013 7.4 -83 160.0 213 347 0.62 0.1203 0.0012 6.0 -84 54.2 84.6 132 0.64 0.1113 0.0014 5.0 -85 30.4 56.5 70.9 0.80 0.1136 0.0018 5.3 -86 111.2 68.5 250 0.27 0.1270 0.0014 5.0 -87 80.5 84.9 143 0.59 0.1276 0.0014 5.7 -88 44.90 36.6 97.4 0.38 0.1276 0.0014 7.7 -88 44.90 36.6 97.4 0.38 0.1276 0.0014 7.7 -90 149.3 102	- 79	79.1	93.5	154	0.61	0.1324	0.0015	7.4413	0.0910	0.4038	0.0029	2131	20	2166	11	2187	13	%66
-81 173.4 174 320 0.54 0.1476 0.0014 9.0 -82 150.7 227 284 0.80 0.1346 0.0013 7.3 -83 160.0 213 347 0.62 0.1203 0.0012 6.0 -84 54.2 84.6 132 0.64 0.1113 0.0012 6.0 -85 30.4 56.5 70.9 0.80 0.1136 0.0014 5.0 -86 111.2 68.5 70.9 0.80 0.1136 0.0014 5.1 -87 80.5 84.9 143 0.59 0.1276 0.0014 6.9 -88 44.90 36.6 97.4 0.38 0.1276 0.0015 6.9 -90 149.3 102 331 0.31 0.1276 0.0014 7.7 -91 58.7 53.0 0.84 0.1355 0.0014 7.7 -92 39.6 60.6 0.74	- 80	105.5	131	236	0.56	0.1191	0.0012	5.9883	0.0654	0.3611	0.0024	1943	19	1974	10	1987	11	%66
-82 150.7 227 284 0.80 0.1346 0.0013 7. -83 160.0 213 347 0.62 0.1203 0.0012 6. -84 54.2 84.6 132 0.64 0.1113 0.0014 5. -85 30.4 56.5 70.9 0.80 0.1136 0.0014 5. -86 111.2 68.5 250 0.27 0.1770 0.0016 9. -87 80.5 84.9 143 0.59 0.1276 0.0016 9. -88 44.90 36.6 97.4 0.38 0.1276 0.0016 9. -89 86.3 134 159 0.84 0.1355 0.0014 7. -90 149.3 102 331 0.31 0.1276 0.0014 7. -91 58.7 53.0 112 0.47 0.1448 0.0016 8. -91 58.7 53.0 0.121 0.0013 6. 9. 9. 9. 9. 9. 9.	- 81	173.4	174	320	0.54	0.1476	0.0014	9.0175	0.0919	0.4386	0.0028	2318	21	2340	6	2344	12	%66
-83 160.0 213 347 0.62 0.1203 0.0012 6.0 -84 54.2 84.6 132 0.64 0.1113 0.0014 5.0 -85 30.4 56.5 70.9 0.80 0.1136 0.0014 5.0 -86 111.2 68.5 250 0.27 0.1270 0.0014 5.0 -87 80.5 84.9 143 0.59 0.1270 0.0016 91. -88 44.90 36.6 97.4 0.38 0.1276 0.0015 61. -89 86.3 134 159 0.84 0.1355 0.0014 7. -90 149.3 102 331 0.31 0.1276 0.0014 7. -91 58.7 53.0 112 0.31 0.1248 0.0016 8.0 -92 39.6 65.7 0.31 0.31 0.1448 0.0015 5.7	- 82	150.7	227	284	0.80	0.1346	0.0013	7.4881	0.0761	0.3989	0.0024	2159	17	2172	6	2164	11	%66
-84 54.2 84.6 132 0.64 0.1113 0.0014 5.0 -85 30.4 56.5 70.9 0.80 0.1136 0.0014 5.0 -86 111.2 68.5 250 0.27 0.1270 0.0014 5.0 -87 80.5 84.9 143 0.59 0.1507 0.0016 9.5 -88 44.90 36.6 97.4 0.38 0.1276 0.0015 6.9 -89 86.3 134 159 0.84 0.1355 0.0014 7.7 -90 149.3 102 331 0.31 0.1276 0.0014 7.7 -91 58.7 53.0 112 0.47 0.1448 0.0013 6.8 -92 39.6 60.6 95.7 0.63 0.1103 6.9 5.7	- 83	160.0	213	347	0.62	0.1203	0.0012	6.0871	0.0616	0.3630	0.0020	1961	23	1988	6	1996	10	%66
-85 30.4 56.5 70.9 0.80 0.1136 0.0018 5.3 -86 111.2 68.5 250 0.27 0.1270 0.0014 6.6 -87 80.5 84.9 143 0.59 0.1507 0.0016 9.3 -88 44.90 36.6 97.4 0.38 0.1276 0.0015 6.9 -89 86.3 134 159 0.84 0.1355 0.0014 7.3 -90 149.3 102 331 0.31 0.1271 0.0013 6.8 -91 58.7 53.0 112 0.47 0.1448 0.0016 8.6 -92 39.6 60.6 95.7 0.63 0.1103 6.8 6.8	- 84	54.2	84.6	132	0.64	0.1113	0.0014	5.0491	0.0645	0.3255	0.0022	1820	22	1828	11	1816	11	%66
-86 111.2 68.5 250 0.27 0.1270 0.0014 6.2 -87 80.5 84.9 143 0.59 0.1507 0.0016 9.2 -88 44.90 36.6 97.4 0.38 0.1276 0.0015 6.9 -89 86.3 134 159 0.84 0.1355 0.0014 7. -90 149.3 102 331 0.31 0.1271 0.0013 6.3 -91 58.7 53.0 112 0.47 0.1448 0.0015 8.0 -92 39.6 65.7 0.63 0.1103 0.015 5.1	- 85	30.4	56.5	70.9	0.80	0.1136	0.0018	5.3533	0.0895	0.3403	0.0033	1858	29	1877	14	1888	16	%66
-87 80.5 84.9 143 0.59 0.1507 0.0016 9.1507 -88 44.90 36.6 97.4 0.38 0.1276 0.0015 6.9 -89 86.3 134 159 0.84 0.1355 0.0014 7.7 -90 149.3 102 331 0.31 0.1271 0.0013 6.9 -91 58.7 53.0 112 0.47 0.1448 0.0013 6.3 -92 39.6 60.6 95.7 0.63 0.1103 0.015 5.1	- 86	111.2	68.5	250	0.27	0.1270	0.0014	6.7727	0.0780	0.3827	0.0025	2057	18	2082	10	2089	12	%66
-88 44.90 36.6 97.4 0.38 0.1276 0.0015 6.9 -89 86.3 134 159 0.84 0.1355 0.0014 7.7 -90 149.3 102 331 0.31 0.1271 0.0013 6.1 -91 58.7 53.0 112 0.47 0.1448 0.0016 8.0 -92 39.6 60.6 95.7 0.63 0.1103 0.0015 5.1	- 87	80.5	84.9	143	0.59	0.1507	0.0016	9.3012	0.1041	0.4435	0.0029	2353	19	2368	10	2366	13	%66
-89 86.3 134 159 0.84 0.1355 0.0014 7.3 -90 149.3 102 331 0.31 0.1271 0.0013 6.3 -91 58.7 53.0 112 0.47 0.1448 0.0016 8.6 -92 39.6 60.6 95.7 0.63 0.1103 0.015 5.7	- 88	44.90	36.6	97.4	0.38	0.1276	0.0015	6.9153	0.0855	0.3895	0.0028	2066	16	2101	11	2121	13	%66
-90 149.3 102 331 0.31 0.1271 0.0013 6.3 -91 58.7 53.0 112 0.47 0.1448 0.0016 8.6 -92 39.6 60.6 95.7 0.63 0.1103 0.0015 5.7	- 89	86.3	134	159	0.84	0.1355	0.0014	7.7422	0.0859	0.4104	0.0029	2170	17	2202	10	2217	13	%66
-91 58.7 53.0 112 0.47 0.1448 0.0016 8.6 -92 39.6 60.6 95.7 0.63 0.1103 0.0015 5.7	- 90	149.3	102	331	0.31	0.1271	0.0013	6.8407	0.0719	0.3864	0.0023	2058	18	2091	6	2106	11	%66
-92 39.6 60.6 95.7 0.63 0.1103 0.0015 5.	- 91	58.7	53.0	112	0.47	0.1448	0.0016	8.6416	0.1050	0.4291	0.0031	2287	19	2301	11	2302	14	%66
	- 92	39.6	60.6	95.7	0.63	0.1103	0.0015	5.1442	0.0720	0.3354	0.0024	1806	24	1843	12	1865	12	98%
-93 61.9 62.3 119 0.53 0.1415 0.0018 8.	- 93	61.9	62.3	119	0.53	0.1415	0.0018	8.3089	0.1079	0.4230	0.0029	2256	50	2265	12	2274	13	999%

Fe-Cu-REE

U-Pb

Re-Os

1177

 $\mathbf{P}_{\mathbf{D}}$



Fig. 7 Plot of U-Pb concordant curve ²⁰⁷ Pb/²⁰⁶ Pb age frequency and Th/U-²⁰⁷ Pb/²⁰⁶ Pb age diagram of the det

2

Re-Os

Table 2 Re-Os isotope compositions for chalcopyrite from the Yinachang deposit

	187 Re $\times 10^{-9}$	1σ	187 Os $\times 10^{-9}$	1σ	$\begin{array}{c} {\rm Re} \\ \times 10^{ -9} \end{array}$	1σ	$ Os \times 10^{-9} $	1σ	Ма	1σ
YNC1006	562.306	16.269	16. 881	0.314	898. 253	25.989	0.023	0.006	1732	23
10YNC-40	161.659	2.145	4.455	0.061	258. 242	3.426	0.017	0.001	1638	22
6 YNC1010	4.615	0.108	0.118	0.003	7.373	0.172	0.003	0.000	1719	20
10YNC-32	12. 859	0.300	0.366	0.004	20. 541	0.480	0.004	0.000	1690	20
10YNC-41	246.010	30. 390	6.836	0.079	392. 988	48. 547	0.005	0.001	1651	19
YNC1112	4. 388	0.149	0.073	0.005	7.010	0. 239	0.002	0.000	1687	19

5

5.1 U-Pb LA-ICP-MS U-Pb 1 6 CL 7 ²⁰⁷ Pb/ U-Pb $^{206}\mathrm{Pb}$ Th/U-²⁰⁷Pb/²⁰⁶Pb DFH1101 2000 95% 84 $^{207}\,\mathrm{Pb}/^{206}\,\mathrm{Pb}$ $^{207}\,\mathrm{Pb}/^{206}\,\mathrm{Pb}$ 1746 ± 22 Ma 5 2500Ma $2694 \pm 16 \mathrm{Ma}$ 1.75 ~ 1.85Ga 1. 90 ~ 2. 00Ga 2. 20 ~ 2. 35Ga $^{207}\,\mathrm{Pb}/^{206}\,\mathrm{Pb}$ 1796 ± 15Ma n = 16 MSWD = 1.5 2262 ± 12 Ma n = 34 MSWD = 3.5 1800Ma 1960Ma 2270Ma 7bCL 6 Th/U 0.1 $0.4 \sim 1.0$ 7c DFH1102 2500 93 207 Pb/ 206 Pb 95% $1767 \pm 27 \text{Ma}$ $^{207}\,\mathrm{Pb}/^{206}\,\mathrm{Pb}$ 2989 ± 19 Ma 7 2500Ma 1.75 ~1.88Ga 1.90 ~2.00Ga 2.02 ~2.20Ga 2. 30 ~ 2. 40Ga $^{207}\,\mathrm{Pb}/^{206}\,\mathrm{Pb}$ $1796 \pm 9Ma$ n = 19 MSWD = 0.71 1800Ma 1950Ma 2080Ma 2280Ma 7e CL6 Th/U 0.2 0.4 ~1.0 7f U-Pb

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	La	Ce	Pr	PN	Sm	Eu	Gd	Tb	Dy	Но	Er	Tm	Yb	Lu	Z REE	δEu	δСе	La⁄Yb _N	La/Sm _N	Gd/Yb _N	LREE/ HREE
10YNC-31	670	1050	108	340	54.8	29	37.9	5.38	27.4	4.46	10	1.36	6. 2	0.5	2345	1.95	0. 94	72.86	7.69	4.93	24.16
10YNC-41	584	983	101	320	53.1	30. 9	38.9	6.07	32. 1	5.92	14.2	2.04	9.7	0. 94	2182	2. 08	0. 97	40.59	6.92	3.24	18.86
DFH1111	264	421	41.1	128.5	19.5	11.8	12.5	1.63	8.9	1.61	4.4	0.87	5.3	0.57	922	2.31	0. 97	33.58	8.52	1.90	24.76
DFH1112	609	961	97.9	319	52.1	44. 4	42.1	9	31. 2	6. 02	14.3	1.78	8.9	0. 73	2194	2.90	0. 95	46.13	7.35	3.82	18.76
YNC1003	186	340	47.2	179	38.1	26.4	36.8	6.09	35	6.95	17.9	2. 12	11.3	1. 13	934	2. 16	0. 87	11.10	3.07	2.63	6.96
YNC1004	31.2	53.1	5.05	17.1	2.6	3.09	2. 08	0. 23	0.975	0.154 (0.404 0	. 0453 0	. 284 (). 033	116	4.06	1. 02	74.07	7.55	5.92	26.63
YNC1011	144	228	21.4	74.5	14.6	19.8	15.9	2.88	16. 7	3. 74	9.87	1.33 (5.93 (). 783	805	3.97	0. 99	14.01	6.20	1.85	8.64
YNC1015	217	335	29.9	102	18.3	24. 1	20.9	3.86	22. 8	5.38	13.3	1.73 9	9.54	1. 08	560	3.77	1. 00	15.34	7.46	1.78	9. 23
YNC1006	129	279	31.6	124	27.6	10.3	29.5	5.38	31.9	7. 09	18.5	2.34	12	1. 18	709	1.10	1. 05	7.25	2.94	1.98	5.58
YNC1007	125	249	26.8	99.7	19.5	7.6	19.3	2.98	15.2	2.96	7.24 (). 853 2	4.58 (). 477	581	1.20	1.04	18.40	4.03	3.41	9.84
YNC1008	169	322	41.2	158	25.3	8.55	20.4	3.1	14. 9	3. 31	8.54	1.17 (5.48 (). 747	783	1. 15	0. 93	17.58	4.20	2.55	12.35
YNC1009	2180	4320	525	1890	374	125	320	52.8	320	68.3	159.5	20.7 8	38. 2	8.2	10452	1. 11	0. 97	16.66	3.67	2.93	9.07
YNC1010	251	640	90.9	370	93.7	45.8	93.9	17.4	104	21.4	51.6	5.89	26. 5	2. 45	6223	1.49	1. 02	6.39	1.69	2.86	4.61
YNC1012	382	978	120	572	130	60.7	147	26.9	163	36.3	88.4	10.3	46. 6	4. 36	10736	1.34	1.10	5.53	1.85	2.54	4.29
YNC1013	356	1111	121	496	102	43. 3	97.9	17.7	98.6	20.1	47.3	5.31	23. 8	2. 28	4802	1.32	1. 29	10.08	2.20	3.32	7.12
YNC1014	1060	2423	279	1320	271	87.6	268	43.8	235	48.2	112	12.7	57. 9	5.17	2766	0. 99	1.07	12.34	2.46	3.73	6.95
10YNC-30	2350	4630	558	1970	361	126	274	40.6	223	43.3	94.1	12.3	49.6	4. 35	2542	1. 22	0. 97	31.94	4.09	4.46	13.48
10 YNC-32	1035	2040	24 2																		

 $\times10^{-6}$ Table 3 Rare earth elements REE contents $\times10^{-6}$ of ones and wall-rock form the Yinachang deposit





Fig. 8 Isochrone age diagram a and weighted average of model age b of Re-Os isotope for chalcopyrite of the Yinachang deposit

			2	UFF	= 207							
$\times 10^{-6} \sim 270 \times 1$	0 - 6					17	780Ma			U-Pl	э	1742 ±
	La/Yb	_N 14. 1 ~ 23. 9	La/	Sm _N	4.8	13Ma Zhao		2010				
~7.1 LREE	/HREE	11. 2 ~ 16. 9				U-Pb	169	90 ± 32Ma	Zhao	20	10	
					δEu			1. 7Ga				
= 2. 31 ~ 2. 50		$\delta Ce = 1.1$	3	9c					U-Pb		1711	1 ±4Ma
						2012				U-Pb		1. 7Ga
<i>.</i>							2008	Greentree	e and Li	2008	Zhao	and Zhou
6						2011						1.7Ga
6. 1										U	-Pb	1695
	1954					± 20 Ma		2009				
						$1710 \pm 8 \mathrm{Ma}$		U-Pb			2011	

- 1	990

1993

1995

~ 2280Ma

2. 5Ga

~ 1800Ma ~ 1950Ma ~ 2080Ma

1181

	Zhang	2006 Greentree		
and Li 2008 Zhao 20	010			
LA-ICP-MS U-Pb				
DFH1101		1746 ±		
22Ma	U 1	20×10^{-6} Th		
68. 7 × 10 ⁻⁶	Th/U 0.57			
DFH1102	²⁰⁷ Pb/ ²⁰⁶ Pb	1767 ±		
27Ma U 91×10^{-6} Th	62×10^{-6}	Th/U		
0. 68			6.2	Fe-Cu-REE
$^{207}{ m Pb}/^{206}{ m Pb}$	1750Ma			-
1750Ma				



normalizing values after Boynton 1984

IOCG

7

1 1.7Ga LA-ICP-MS U-Pb 1750Ma 1.7Ga Columbia Rogers and Santosh 2002 2 Fe-Cu-REE Re-Os Zhao 2002 $1690 \pm 99 Ma$ 1.7Ga Columbia Zhao and Zhou 3 2011 Wang 2012 Yu 2012 1.7Ga Fe-Cu

U-Pb

Re-Os

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